

碳纳米材料互连线的单粒子串扰特性研究

刘保军¹, 张 爽¹, 李 成²

(1. 空军工程大学航空机务士官学校, 河南信阳 464000;
2. 国防科技大学计算机学院高性能计算国家重点实验室, 湖南长沙 410073)

摘要: 碳纳米材料互连线由于其良好的电学、热学和力学特性, 成为研究热点. 随着技术节点的缩减, 串扰效应对电路的影响愈加显著. 本文针对单壁碳纳米管束(Single Walled Carbon Nanotube Bundles, SWCNT)、多壁碳纳米管束(Multi Walled Carbon Nanotube Bundles, MWCNT)、单层石墨烯(Single Layer Graphene Nano-Ribbon, SLG NR)及多层石墨烯(Multi Layer Graphene Nano-Ribbon, MGLNR)的互连线, 研究了统一的等效RLC模型, 并构建了单粒子串扰(SEC)的等效电路, 对比分析了四种互连线在32 nm, 21 nm和14 nm技术节点下的SEC峰值电压和脉冲宽度. 结果表明, 与铜互连线相比, 碳纳米材料互连线的SEC较弱, 但对传输信号的衰减作用较大, 综合信号衰减和耦合作用程度, SWCNT和MLG NR更能有效抑制SEC的传播和影响. 最后, 本文利用灰色理论, 分析了SEC与RLC参数之间的潜在关联性.

关键词: 碳纳米管; 石墨烯; 互连线; 单粒子串扰

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Research on Single Event Crosstalk Characteristic of Carbon Nanomaterial Interconnects

LIU Bao-jun¹, ZHANG Shuang¹, LI Cheng²

(1. Aviation Maintenance NCO Academy, Air Force Engineering University, Xinyang, Henan 464000, China;
2. Institute for Quantum Information & State Key Laboratory of High Performance Computing, College of Computer, National University of Defense Technology, Changsha, Hunan 410073, China)

Abstract: Due to its well electrical, thermal and mechanical properties, carbon nanomaterial interconnect has become a research hotspot. As devices feature sizes scale down into nano meter, single event transient (SET) becomes the most serious threat for the reliability of integrated circuits (ICs) with advanced process in the future, which should be highly concerned. With CMOS technology scaling continuing and operating frequencies increasing, SET might bring noise into electronically unrelated multiple logic circuit paths due to increased crosstalk effects between interconnects, which can intensify the SET susceptibility of nanometer CMOS circuits. Therefore, single event crosstalk (SEC) effects should be considered carefully in the early design stages of circuits applied for space and ground radiation environments. As technology nodes scaled down, the impact of crosstalk effects on the integrated circuits becomes more and more significant. Although many works have been carried out on the crosstalk effect of carbon nanomaterial interconnects, the conclusions obtained cannot well guide the analysis and research of the radiation effect of integrated circuits of carbon nanomaterial interconnects. For single-walled carbon nanotube bundles (SWCNT), multi-walled carbon nanotube bundles (MWCNT), single-layer graphene (SLG NR) and multilayer graphene (MGLNR) interconnects, a unified equivalent RLC model is studied. The equivalent circuit of single event crosstalk (SEC) is built. The SEC peak voltage and pulse width of four interconnects at 32 nm, 21 nm and 14 nm technology nodes are compared and analyzed. The results show that, compared with the copper interconnect, the SEC of the carbon nanomaterial interconnects is smaller, but has a greater attenuation effect on the transmission signal. This results in a lower peak voltage and a larger pulse width of SEC. With the technology node scaling down from 32 nm to 14 nm, the peak voltage of SEC tends to increase, and the pulse width of SEC changes insignificantly, except for SWCNT and MLG NR. The peak voltage of SEC in SWCNT interconnect is increased by 2.88 times and the pulse width is reduced by 1.56 times. The peak voltage of SEC in MLG NR is very low, and the pulse width is higher, and almost un-

changed. Comprehensive signal attenuation and coupling degree, the performance of SWCNT and MLGNR is better. They can effectively suppress the propagation and influence of crosstalk. Finally, using grey theory, the potential correlation between SEC and RLC parameters is analyzed. The results show that the coupling capacitance and distributed inductance of interconnects will affect the peak voltage and pulse width to a large extent. Therefore, in the early stage of the circuit design, it is necessary to consider how to layout to reduce the coupling capacitance and inductance, thereby reducing crosstalk noise. These results will provide technical supports and ideas for the optimal design and evaluation of carbon nano interconnects applications in radiation dedicated circuits.

Key words: carbon nanotube; graphene; interconnect; single event crosstalk

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1 引言

随着器件特征尺寸进入纳米尺度,传统铜互连线电阻率过大等问题愈发严重.新型的碳纳米材料,如碳纳米管、石墨烯等^[1,2],具有良好的电学、热学和力学特性,被认为是很有潜力的互连材料.同时,互连线的间隔宽度比缩小、厚宽比增加,导致互连线间的耦合效应增强.故在先进电路芯片设计流水线和信号完整性分析的早期阶段,必须考虑互连线间串扰效应的影响^[3,4].

在辐射环境中,高能粒子会诱发单粒子瞬态(Single Event Transient, SET),形成软错误.SET已成为纳米工艺电路须重点关注的辐射效应.串扰效应可使SET影响不相关路径的电路,从而增加其SET易受攻击部分和敏感性.故单粒子串扰(Single Event Crosstalk, SEC)的分析和预测是一项非常重要的研究工作^[5,6].

针对串扰效应,研究人员已开展了大量工作,如用时域有限差分法、ABCD矩阵法、谱域随机法等进行串扰的预测、延时估计等^[7-10],分析温度、频率等对串扰的影响等^[11-15].针对SEC, Balasubramanian等^[16]利用90 nm的单个和两个光子激光吸收技术,测试并证实了SEC的存在; Sayil等^[3,6]基于互连线的 $4-\pi$ 分布RC网络模型,提出了一种SEC预测模型,平均误差约6.16%,并

分析了温度的影响;Liu等^[4,17,18]基于导纳规则,建立了SEC的估计模型,平均误差3.07%,并建立了多线间SEC的预测模型,平均误差5.52%;综合考虑寄生容性和感性效应,构建了SEC解析模型,预测误差为2.19%.以上研究均是针对铜互连线的,尚缺乏新型碳纳米材料互连线的SEC的相关研究.虽然研究人员针对碳纳米材料互连的串扰效应开展了一些研究,但系统性不强,得到的结论并不能很好地指导集成电路的辐射效应分析和研究.因此,迫切需要开展新型碳纳米材料互连线的SEC相关研究.

2 互连线的等效RLC模型

本文碳纳米材料互连线是金属性的,主要考虑四种类型^[1,2,7-9,12,13,19-22]:单壁碳纳米管束(Single Walled Carbon Nanotube bundle, SWCNT)、多壁碳纳米管束(Multi-Walled Carbon Nanotube bundle, MWCNT)、单层石墨烯(Single Layer Graphene Nano-Ribbon, SLGNR)及多层石墨烯(MultiLayer Graphene Nano-Ribbon, MLGNR),如图1所示.其中, w, h, l 分别表示互连线的宽度、厚度和长度, s 是两线间隔, h_i 是距地面高度,互连线与地面之间是介质材料, D 是单壁碳纳米管直径, D_{\min} 和 D_{\max} 分别是多壁碳纳米管的最小和最大直径, $\delta=0.34$ nm是范德华距离.

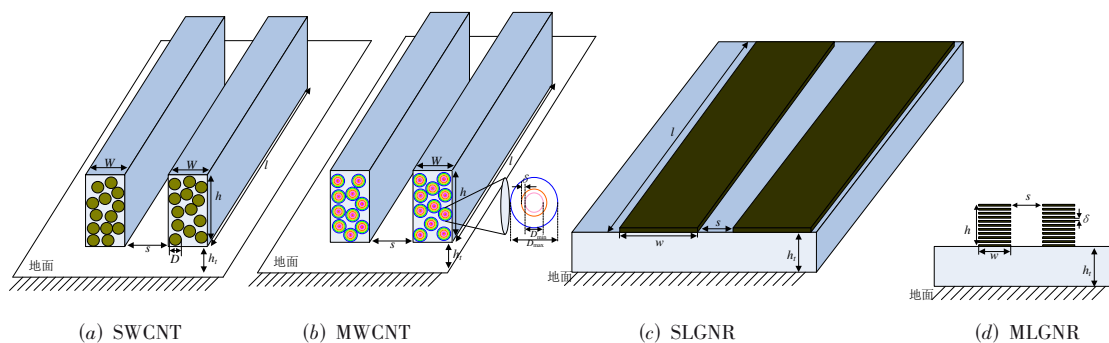


图1 碳纳米材料互连线结构示意图

这里将碳纳米互连线等效为单导体(Equivalent Single Conductor, ESC),即将其各方面的影响都转化为电阻、电容和电感三种参数来考量,同时,考虑到各参数的影响因素的不同,提取的等效电路参数分为集总和分

布参数两类^[2,7,12,19].图2为提取的碳纳米材料互连线的等效RLC电路模型,其中, R_c, R_q 分别为集总的接触电阻和量子电阻, r_s, l_k, l_m, c_q, c_e 均是分布式参数,分别表示散射电阻、动态电感、磁性电感、量子电容及静电电容.

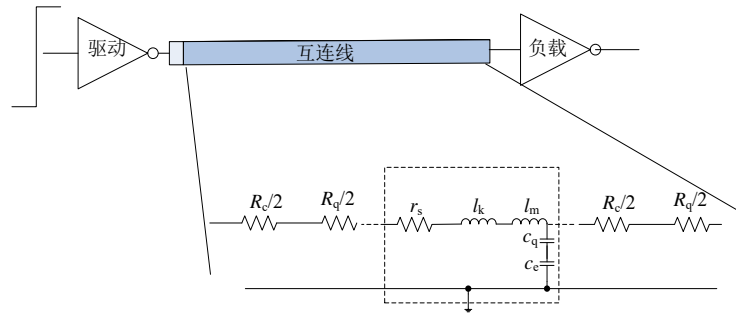


图2 互连线的等效RLC模型

下面分析四种碳纳米材料互连线等效RLC模型中的参数,接触电阻与互连线的材料有很大关系,其值在几百到上千欧之间.通过对四种互连线类型的RLC参数进行归纳总结^[1,2,7-9,12,13,19-22],得到了统一的RLC解析模型,如式(1)和表1所示.

$$R_q = \frac{h_B}{2q^2 N_{\text{cnt}} \sum_{i=1}^N N_i} \quad (1a)$$

$$r_s = \frac{h_B}{2q^2 N_{\text{cnt}} \sum_{i=1}^N N_i \lambda_i(T)} \quad (1b)$$

$$l_k = \frac{h_B}{4q^2 v_F N_{\text{cnt}} \sum_{i=1}^N N_i} \quad (1c)$$

$$l_m = \frac{\mu_0}{2\pi} g(w, h_t) \quad (1d)$$

$$c_q = \frac{4q^2}{h_B v_F} N_x \quad (1e)$$

$$c_e = \epsilon_0 \epsilon_r f(w, h_t) \quad (1f)$$

其中, h_B 是普朗克常数,其值为 $6.625 \times 10^{-34} \text{ J} \cdot \text{s}$, q 是电子电荷,为 $1.602 \times 10^{-19} \text{ C}$, v_F 是费米速度,为 $8 \times 10^5 \text{ m/s}$, μ_0 是真空磁导率,为 $4\pi \times 10^{-7} \text{ H/m}$, ϵ_0 是真空的介电常数,为 $8.854 \times 10^{-12} \text{ F/m}$, ϵ_r 是介质的相对介电常数.

表1 式(1)中的相关参数

参数	互连线类型			
	SWCNT	MWCNT	SLGNR	MLGNR
N_{cnt}	$N_w = \lfloor (w-D)/(D+\delta) \rfloor + 1$	$N_H = \lfloor 2/\sqrt{3} \times (h-D)/(D+\delta) \rfloor + 1$	$N_{\text{cnt}} = P_m (N_H N_w - \lfloor N_H/2 \rfloor)$	1
N	1	$\lfloor (D_{\text{max}} - D_{\text{min}})/(2\delta) \rfloor + 1$		1
N_i	2	$N_i = \begin{cases} aTD_i + b, & D_i > d_T/T \\ 2/3, & D_i > d_T/T \end{cases}$		$aE_F w$
$\lambda_i(T)$	$\lambda_i(T) = (\lambda_{\text{AC}}^{-1} + \lambda_{\text{op,ems}}^{-1} + \lambda_{\text{op,abs}}^{-1})^{-1}$, $\lambda_{\text{op,ems}}(T) = [\lambda_{\text{op,ems}}^{\text{fd}}(T)^{-1} + \lambda_{\text{op,ems}}^{\text{abs}}(T)^{-1}]^{-1}$			
	$\lambda_{\text{op,ems}}^{\text{abs}}(T) = \lambda_{\text{op,abs}} + \lambda_{\text{op}}^{\text{fd}}$, $\lambda_{\text{op,ems}}^{\text{fd}}(T) = y(T)/V_{DD} + \lambda_{\text{op}}$, $N_{\text{OP}}(T) = \frac{1}{\exp(\frac{h_{\text{B,op}}}{k_B T}) - 1}$			
$\lambda_i(T)$	$\lambda_{\text{AC}} = 1600 \times (\frac{300}{T})$	$\lambda_{\text{AC}} = \frac{4 \times 10^5 D_i}{T}$	$\lambda_{\text{AC}} = \frac{\rho_m (h_B / \pi v_F v_s)^2}{\sqrt{\pi N_s} D_{\text{AC}}^2 k_B T}$	
	$\lambda_{\text{op}} = 15 \times \frac{N_{\text{OP}}(300) + 1}{N_{\text{OP}}(T) + 1}$	$\lambda_{\text{op}} = 56 D_i \frac{N_{\text{OP}}(300) + 1}{N_{\text{OP}}(T) + 1}$	$\lambda_{\text{op,abs}} = \frac{\rho_m h_{\text{B,op}} v_F^2}{\sqrt{\pi N_s} D_{\text{op}}^2 N_{\text{OP}} (1 + \frac{2\pi h_{\text{B,op}}}{h_B v_F \sqrt{\pi N_s}})}$	
$\lambda_i(T)$	$\lambda_{\text{op,abs}} = 15 \times \frac{N_{\text{OP}}(300) + 1}{N_{\text{OP}}(T)}$	$\lambda_{\text{op,abs}} = e^{\frac{h_{\text{B,op}}}{k_B T}} \lambda_{\text{op}}$	$\lambda_{\text{op,ems}} = \frac{\rho_m h_{\text{B,op}} v_F^2}{\sqrt{\pi N_s} D_{\text{op}}^2 N_{\text{OP}} (1 - \frac{2\pi h_{\text{B,op}}}{h_B v_F \sqrt{\pi N_s}})}$	
	$y(T) = \frac{h_{\text{B,op}}}{q}$	$y(T) = \frac{h_{\text{B,op}} - k_B T}{q}$		
$g(w, h_t)$	$\frac{1}{N_w} \cosh^{-1}(\frac{D+2h_t}{D})$		$\cosh^{-1}(\frac{h_t}{w})$	$\frac{2\pi h_t}{w}$
N_x	$N_{\text{cnt}} \sum_{i=1}^N N_i$			$\frac{1}{2} \alpha w E_F (1 + \sqrt{1 + 1/\alpha \beta E_F})$
$f(w, h_t)$	$\frac{2\pi N_w}{\cosh^{-1}(\frac{D+2h_t}{D})}$		$M(\tanh(\frac{\pi w}{h_t}))$	$\frac{w}{h_t}$

表 1 中未加说明的 D 均指最大直径, MLGNR 的动态电感 l_k 需利用迭代的方法得到^[1], k_B 是玻尔兹曼常数, 为 1.38×10^{-23} J/K, $a = 2.04 \times 10^{-4}$ nm⁻¹ · K⁻¹, $b = 0.425$, $d_1 = 1\ 300$ nm · K, $\alpha = 1.2$ eV⁻¹ · nm⁻¹, $\beta = 2.3$ nm, $h_{B,op} = 0.18$ eV, $\rho_m = 7.6 \times 10^{-7}$ kg/m², $v_s = 20$ km/s, $N_s = 4 \times 10^{16}$ m², $D_{AC} = 8$ eV, $D_{op} = 2 \times 10^{11}$ eV/m, $\lfloor \cdot \rfloor$ 表示向下取整, N_{cnt} 是导电管(层)数, N 是单根(层)导线的导电沟道数, $\lambda_i(T)$ 是温度为 T 时, 第 i 个导电沟道中的电子平均自由程, D_i 是单根 MWCNT 第 i 层的直径, P_m 是导线管束中金属性碳纳米管的比例, E_F 是费米能级, V_{DD} 是加载电压, $M(x)$ 是一个分段函数, 表达式如下:

$$M(x) = \begin{cases} 2\pi \left[\ln \left(2 \times \frac{1 + \sqrt[4]{1-x^2}}{1 - \sqrt[4]{1-x^2}} \right) \right]^{-1}, & 0 \leq x < \frac{1}{\sqrt{2}} \\ \frac{2}{\pi} \ln \left(2 \times \frac{1 + \sqrt{x}}{1 - \sqrt{x}} \right), & \frac{1}{\sqrt{2}} \leq x \leq 1 \end{cases} \quad (2)$$

3 SEC 等效电路

高能粒子诱发的 SET, 在电路分析中通常采用在敏感结点引入瞬态双指数电流源来表征^[4], 表达式为

$$I(t) = \frac{Q_{dep}}{\tau_\alpha - \tau_\beta} (e^{-t/\tau_\alpha} - e^{-t/\tau_\beta}) \quad (3)$$

其中, Q_{dep} 是粒子入射的累积电荷量, τ_α 是 p-n 结的电荷

收集时间常数, τ_β 是粒子轨迹初始化建立的时间常数. 这里的 τ_α 和 τ_β 分别设置为 50 ps 和 1 ps.

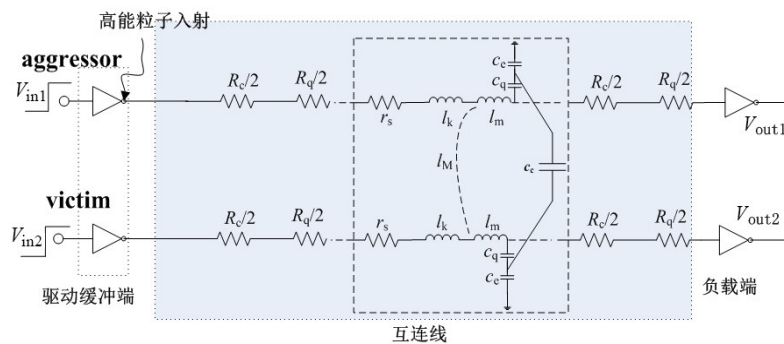
针对反相器链, 通过两根耦合碳纳米材料互连线来分析 SEC, 原始电路图如图 3(a) 所示. 将互连线等效为 RLC 的分布式网络(图 2), 驱动反相器缓冲端等效为 RC 并联网路, 负载端等效为电容, 施扰线加载 SET 瞬态电流源, 受扰线保持静止, 构建的 SEC 等效电路如图 3(b) 所示, 基于 ESC 和保角变换方法得到耦合电容 c_c 和耦合电感 l_m 的表达式^[12,19,20,22], 如式(4)所示, 式中耦合电容和电感的上标分别对应 SWCNT, MWCNT, SLGNR 和 MLGNR 等四种互连线的耦合电容和电感.

$$c_c^{SWCNT} = \frac{N_w - 2}{2} \frac{2\pi\epsilon_0\epsilon_r}{\ln\left(\frac{s+w}{D}\right)} + \frac{3N_H + 4}{5} \frac{2\pi\epsilon_0\epsilon_r}{\ln\left(\frac{s}{D}\right)} \quad (4a)$$

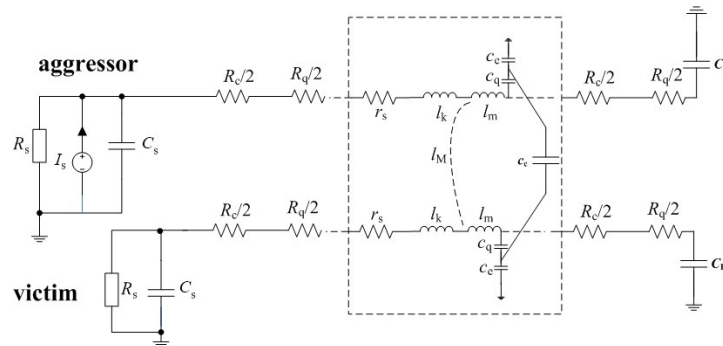
$$c_c^{MWCNT} = \frac{\pi\epsilon_0\epsilon_r N_{cnt}}{\ln\left(\frac{s}{D_{max}} + \sqrt{\left(\frac{s}{D_{max}}\right)^2 + 1}\right)} \quad (4b)$$

$$c_c^{SLGNR} = \frac{\epsilon_0\epsilon_r}{4} M\left(\sqrt{1 - (1 + 2w/s)^{-2}}\right) \quad (4c)$$

$$c_c^{MLGNR} = \left(\frac{0.5}{1 + s^2/(h_t + h)^2} C_{[BCP]} \left(\frac{h}{s/2}, \frac{2d}{s/2} \right) + \frac{0.87}{1 + (s/2)^2/(h_t + h)^2} C_{[CP]}(w/s) \right) \quad (4d)$$



(a) 原始电路



(b) 等效电路

图 3 SEC 等效电路

$$I_M^{SWCNT/MWCNT} = \frac{1}{N_H} \frac{\mu_0}{2\pi} \left[\ln \left(\frac{l}{s+D} + \sqrt{1 + \left(\frac{l}{s+D} \right)^2} \right) + \frac{s+D}{l} - \sqrt{1 + \left(\frac{s+D}{l} \right)^2} \right] \quad (4e)$$

$$I_M^{MLGNR} = \frac{\mu_0}{2\pi} \left[\ln \left(\frac{l}{s+w} + \sqrt{1 + \left(\frac{l}{s+w} \right)^2} \right) + \frac{s+w}{l} - \sqrt{1 + \left(\frac{s+w}{l} \right)^2} \right] \quad (4f)$$

其中,SLGNR的 I_M 忽略不计,函数 $C_{[BCP]}(z,y)$ 和 $C_{[CP]}(x)$ 见文献[22].

4 仿真与分析

针对四种碳纳米材料互连线系统,设置技术节点分别为32 nm,21 nm和14 nm,互连线为全局型,相关参数设置参考ITRS-2013.为了对比分析性能,同时仿真了同技术节点下的铜互连的RLC分布模型^[23],并考虑了纳米尺度下铜电阻率的变化^[1].

下面是SEC脉冲宽度和峰值电压的定义^[24].设高能粒子作用下,负载端得到的输出电压为 $V_{out}(t)$,则有效脉冲宽度为

$$W_{SEC} = \frac{\int_0^\infty tV_{out}(t)dt}{\int_0^\infty V_{out}(t)dt} \quad (5)$$

峰值电压为

$$V_{peak} = \frac{\int_0^\infty V_{out}(t)dt}{W_{SEC}} = \frac{\left(\int_0^\infty V_{out}(t)dt \right)^2}{\int_0^\infty tV_{out}(t)dt} \quad (6)$$

随着器件特征尺寸的不断缩减,很小的累积电荷(几fC)也可诱发显著的瞬态电流.设置粒子入射的累积电荷

量为9.8fC,互连线的长度为200 μm,利用SPICE仿真SEC电路,通过式(5)和式(6)计算不同技术节点、不同互连线类型的SEC峰值电压和脉冲宽度,结果如图4和表2所示.

表2 不同互连线的SEC的传输系数

互连线类型		施扰线远端/ 施扰线近端		受扰线远端/ 施扰线远端	
		峰值电压	脉冲宽度	峰值电压	脉冲宽度
Cu	32 nm	0.936 9	1.064 1	0.611 0	1.158 5
	21 nm	0.856 8	1.155 6	0.659 9	1.127 2
	14 nm	0.597 9	1.584 7	0.759 0	1.067 3
SWCNT	32 nm	0.934 1	1.053 3	0.634 6	0.697 8
	21 nm	0.890 7	1.084 3	0.600 3	0.695 8
	14 nm	0.756 0	1.190 2	0.697 2	0.804 9
MWCNT	32 nm	0.730 8	1.305 9	0.879 2	1.045 3
	21 nm	0.726 9	1.317 0	0.843 0	1.058 4
	14 nm	0.432 7	1.988 1	0.954 8	1.012 5
SLGNR	32 nm	0.168 9	5.870 1	0.266 2	1.233 9
	21 nm	0.162 6	6.069 5	0.244 8	1.207 5
	14 nm	0.140 0	7.057 5	0.295 2	1.216 0
MLGNR	32 nm	0.894 0	1.088 6	0.040 5	0.616 8
	21 nm	0.846 1	1.130 5	0.033 2	0.635 0
	14 nm	0.775 2	1.233 8	0.042 4	0.659 6

由图4可见,与铜互连线相比,碳纳米材料互连线的SEC峰值电压较低,而脉冲宽度则偏高,且随着技术节点的缩减,SEC峰值电压呈增加趋势,而脉冲宽度变化不显著.但SWCNT和MLGNR是例外.当技术节点从32 nm缩减到14 nm时,SWCNT的峰值电压增加2.88倍、脉冲宽度减少1.56倍,MLGNR的峰值电压非常低,脉冲宽度比较高,且几乎无变化,其原因是SWCNT的耦合电容变化显著,而MLGNR的 c_c 变化不显著.由表2可知,随着技术节点的缩减,互连线的阻抗增加,对信号传输的衰减作用增强,导致施扰线远端与其近端的峰值电压

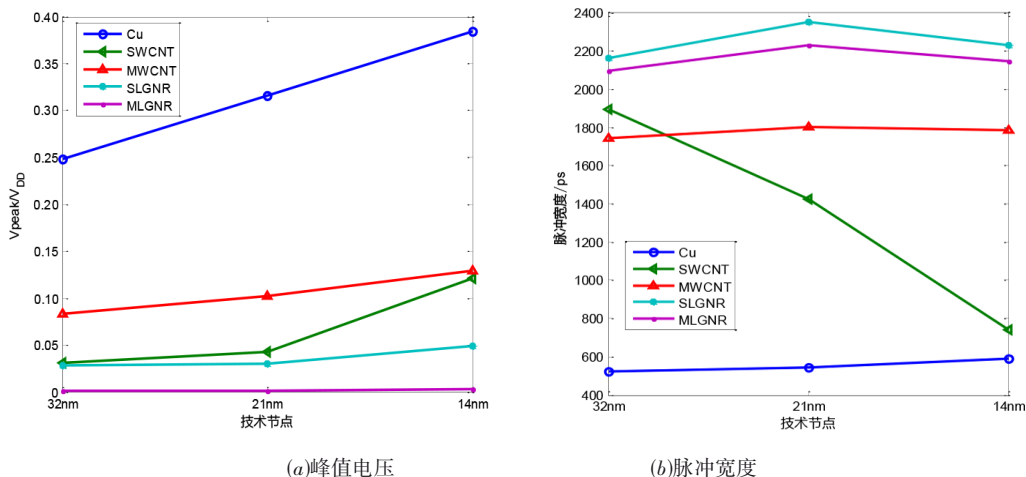


图4 不同技术节点、不同互连线类型的SEC

比值呈显著减小趋势,但 SLG NR 和 MLG NR 的峰值电压比值变化相对较小,同时,较长的 SLG NR 传播信号时,对信号的衰减作用较为严重,故其并不适合作为长互连线来传输信号. 结合受扰线与施扰线远端的峰值电压比值来看,两线间的耦合程度由高到低为 MWCNT, Cu, SWCNT, SLG NR, MLG NR. 因此,由于 SLG NR 和 MWCNT 的信号衰减作用较强,结合耦合程度的差异,最终导致图 4 中的 SWCNT, SLG NR 及 MLG NR 的峰值电压偏低. 对于脉冲宽度而言,信号在

互连线的传播,均会一定程度地展宽脉冲,但 SWCNT 和 MLG NR 的耦合程度相对较低,串扰脉宽比值偏小. 综合信号的衰减程度和耦合效应,SWCNT 和 MLG NR 更能有效抑制串扰的传播和影响.

为了深入分析 SEC 等效电路中 RLC 参数(图 2),与峰值电压及脉冲宽度之间的潜在关联性,设置不同技术节点、不同互连线长度,获取相应的峰值电压和脉冲宽度,利用灰色理论^[25],计算它们的综合关联度,分析潜在的关联性,结果如表 3 所示.

表 3 互连线 RLC 参数与 SEC 间的灰色综合关联度

参数		R_c+R_q	r_s	l_k+l_m	$c_c c_q / (c_c + c_q)$	c_c	l_M
峰值电压	32 nm	0.760 1	0.849 9	0.866 8	0.990 1	0.932 2	0.602 2
	21 nm	0.761 9	0.837 1	0.858 0	0.987 3	0.928 4	0.599 6
	14 nm	0.769 0	0.820 8	0.845 0	0.911 9	0.937 8	0.588 1
脉冲宽度	32 nm	0.756 8	0.926 4	0.956 1	0.886 2	0.944 1	0.602 3
	21 nm	0.757 2	0.922 4	0.963 4	0.883 1	0.927 0	0.599 6
	14 nm	0.759 1	0.898 7	0.949 2	0.827 2	0.908 3	0.588 2

由表可知,峰值电压与分布电感(l_k+l_m)、电容($c_c c_q / (c_c+c_q)$)和耦合电容(c_c)之间存在较高的关联,脉冲宽度与分布电阻(r_s)、电感(l_k+l_m)和耦合电容(c_c)之间存在较高的关联,且关联程度随技术节点的缩减呈减小趋势,而峰值电压和脉冲宽度,与互感(l_M)及集总电阻(R_c+R_q)的关联程度偏弱. 综合上述分析,耦合电容和分布电感在很大程度上会同时影响峰值电压和脉冲宽度,因此,在电路设计时,要考虑如何布局来降低耦合电容及电感,进而达到降低串扰噪声的目的.

5 结论

碳纳米材料互连线具有很好的电学、热学和力学特性,被认为具有潜力应用的互连材料. 随着器件特征尺寸的不断缩减,单粒子瞬态(SET)已成为辐射环境中集成电路软错误的主要来源,严重威胁着电路的可靠性. 不断增强的互连线耦合效应,进一步恶化了 SET 对电路的影响. 本文对 SWCNT, MWCNT, SLG NR 和 MLG NR 等四种新型的碳纳米材料互连线,构建了统一的 RLC 等效模型及其单粒子串扰(SEC)等效电路模型,通过分析 32 nm, 21 nm 及 14 nm 技术节点下 SEC 的峰值电压和脉冲宽度,探讨了四种新型互连线对 SEC、信号传输的影响,并基于灰色关联理论,分析了 RLC 参数与 SEC 之间潜在的关联性,对比分析了四种碳纳米互连材料的 SEC 特点,为碳纳米互连线在辐射专用电路中应用的优化设计和评估提供技术支撑和思路.

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作者简介



刘保军 男, 1984 年生, 山西灵丘人. 博士, 副教授. 主要研究方向为微纳电路系统可靠性、战伤抢修研究.

E-mail: liubaojun102519@sina.com



张爽 男, 1981 年生, 河南信阳人. 副教授. 主要研究方向为可靠性研究、飞机战伤抢修理论与技术研究.

李成 男, 1993 年生, 湖北恩施人. 博士研究生. 主要研究方向为新型信息器件.